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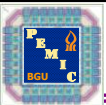
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Prof. Mor M. Peretz

The Center for Power Electronics and Mixed-Signal IC
 Department of Electrical and Computer Engineering
 Ben-Gurion University of the Negev, *ISRAEL*

Emails: morp@bgu.ac.il

Website: <http://www.ee.bgu.ac.il/~pemic>
<http://www.ee.bgu.ac.il/~analog>



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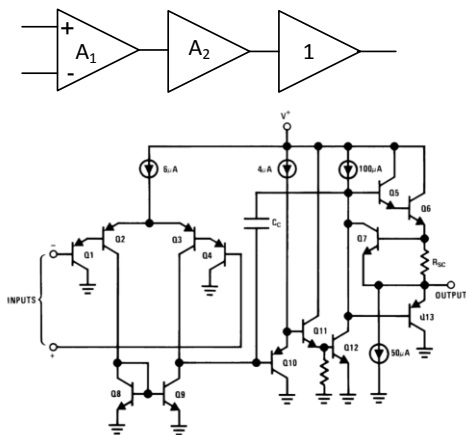
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Lesson #3 Outline

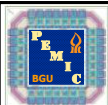
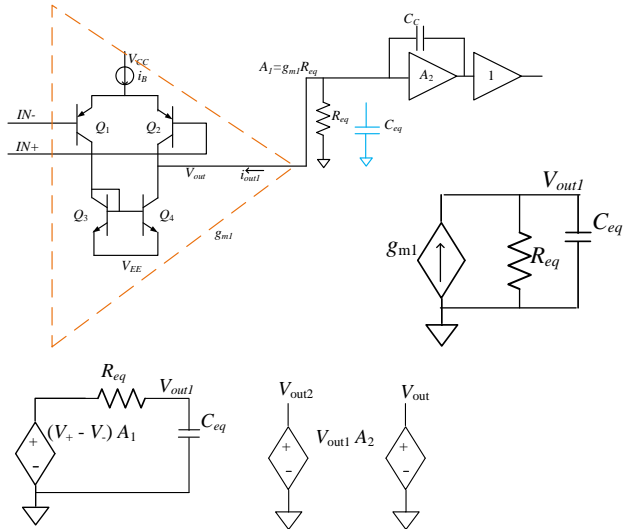
- Dynamic limitations of OpAmps
 - Open-loop response
 - Gain-Bandwidth product
- Drawing A_{OL} , $1/\beta$, βA_{OL}
- Closed-loop response
 - The GBW trade-off
 - Resistive circuits
 - Frequency-dependent circuits
- Transient response
 - Slew-rate



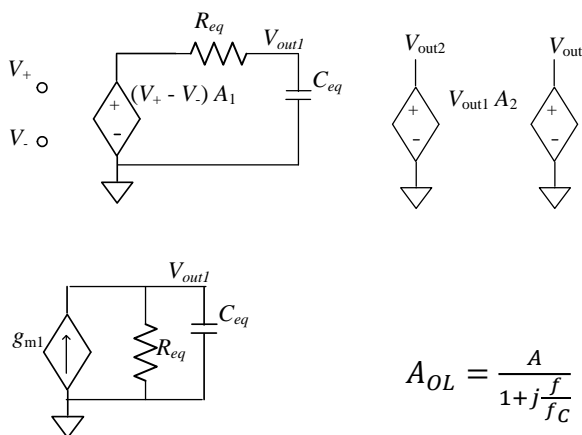
Open-loop response



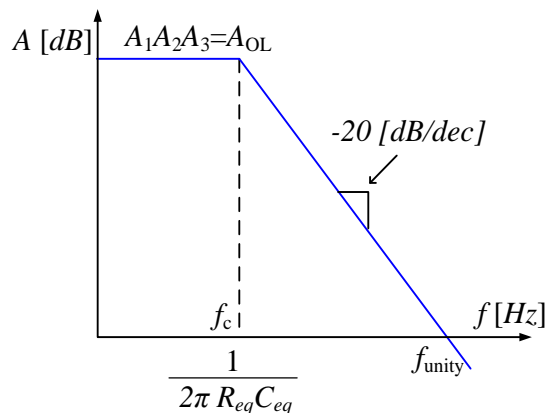
LM324 (Texas Instruments, National)



Open-loop response



$$A_{OL} = \frac{A}{1 + j\frac{f}{f_c}}$$





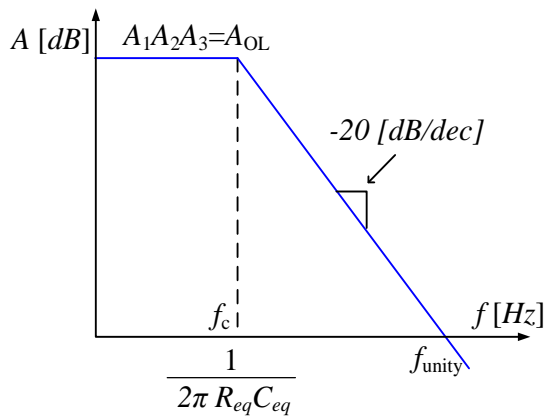
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Gain-Bandwidth Product - GBW



$$A_{CL} = G \frac{A_{OL}}{1 + \beta A_{OL}}$$

$$\beta = 1, G = 1$$

$$A_{CL} = \frac{A_{OL}}{1 + A_{OL}}$$

$$GBW = A_{OL} f_c = f_{unity}$$



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Loop-Gain Nyquist Criterion

$$A_{CL} = G(s) \frac{A_{OL}(s)}{1 + \beta A_{OL}(s)}$$

- The system is unstable if the characteristic equation $\{1 + \beta A_{OL}(s)\}$ has roots in the right half of the complex plane
- Nyquist criterion is a test for location of $\{1 + \beta A_{OL}(s)\}$ roots
- Nyquist criterion can be viewed on the frequency domain (Bode)



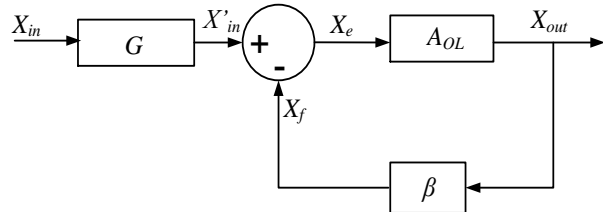
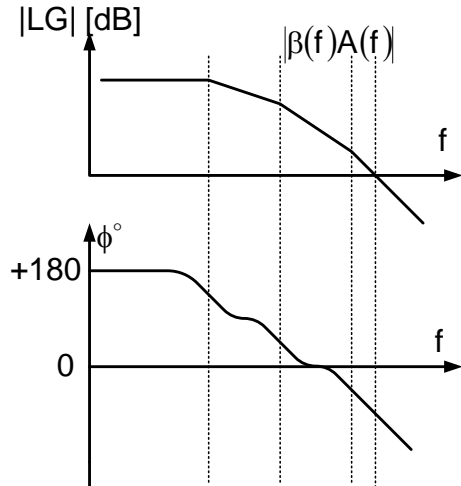
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Loop-gain on the frequency domain



In negative feedback
systems $\phi = 180^\circ (-180^\circ)$
At $f \rightarrow 0$



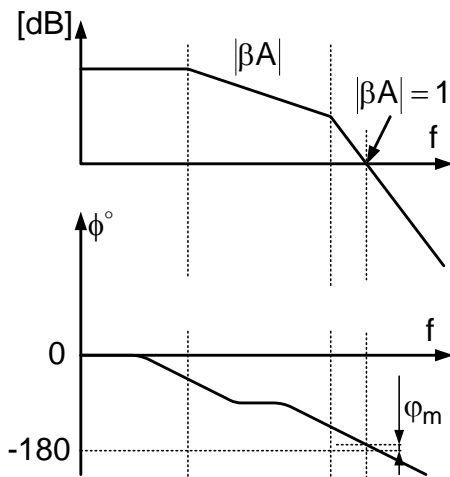
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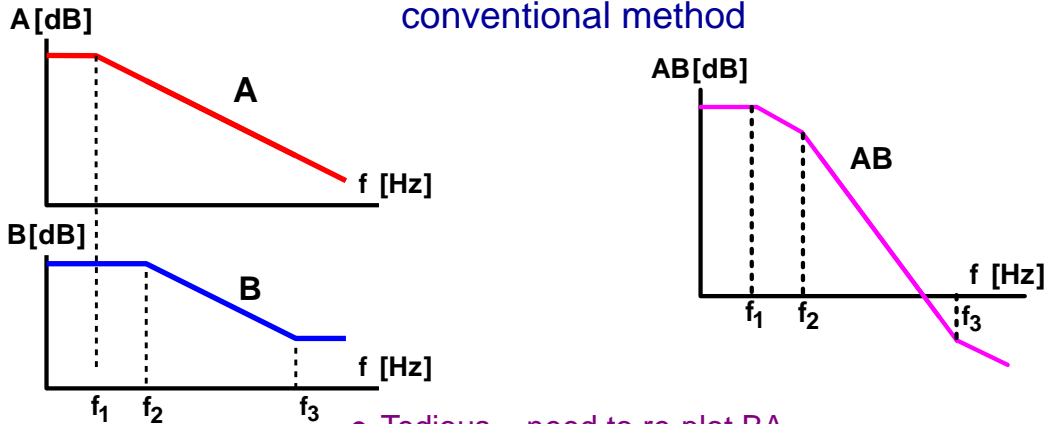
Bode plot Phase margin



$$\phi_m = \phi_{|\beta A|=1} - (-180^\circ) = \phi_{|\beta A|=1} + 180^\circ$$



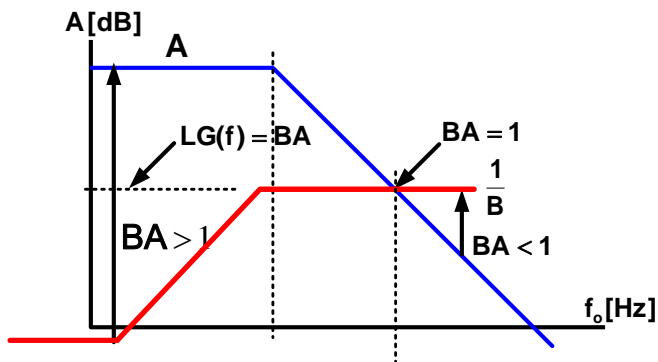
Graphical representation of βA_{OL} conventional method



- Tedious – need to re-plot BA
- Analysis (not design) oriented
- Requires iterations



Graphical Representation of βA_{OL}



$$20\log A - 20\log \frac{1}{B} = 20\log(BA)$$

$$20\log A = 20\log \frac{1}{B} \Rightarrow B \cdot A = 1$$



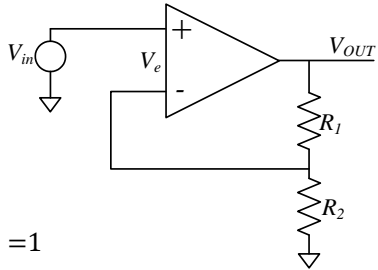
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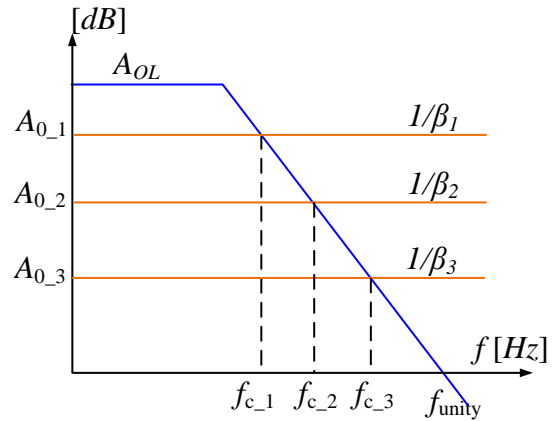
Closed-loop response Non-inverting Amp



$$G = 1$$

$$\frac{1}{\beta} = \frac{R_1 + R_2}{R_2}$$

$$GBW = A_0 f_c = f_{unity}$$



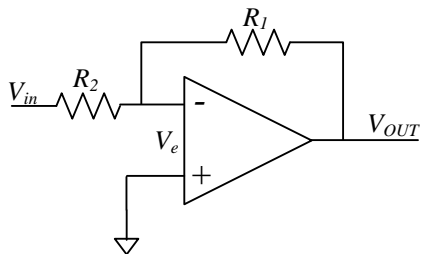
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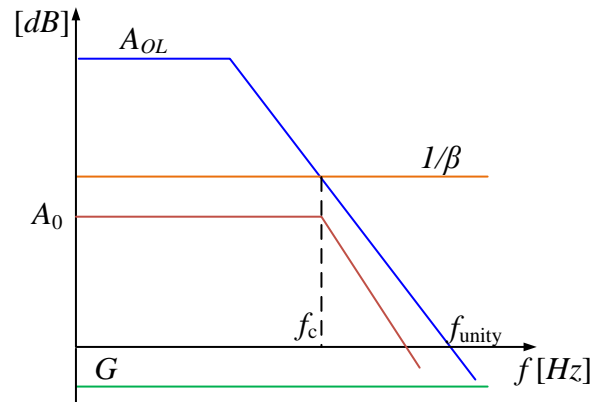
Closed-loop response Inverting Amp



$$G = \frac{R_1}{R_1 + R_2}$$

$$\frac{1}{\beta} = \frac{R_1 + R_2}{R_2}$$

$$GBW = A_0 f_c = f_{unity}$$





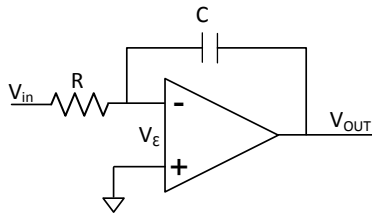
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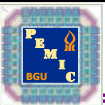
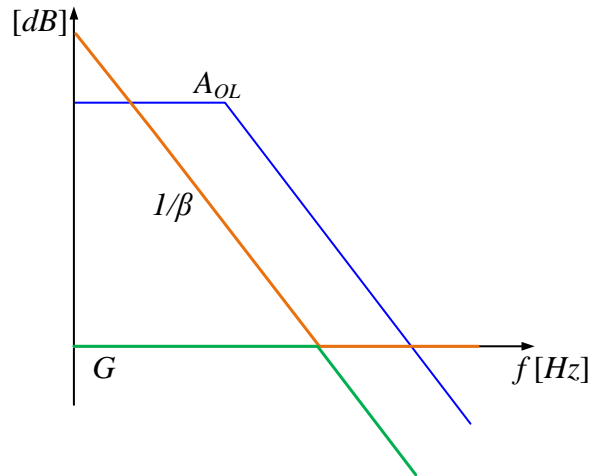
Closed-loop response Integrator



$$G = \frac{1}{sCR + 1}$$

$$\frac{1}{\beta} = \frac{sCR + 1}{sCR}$$

$$GBW = A_0 f_c = f_{unity}$$



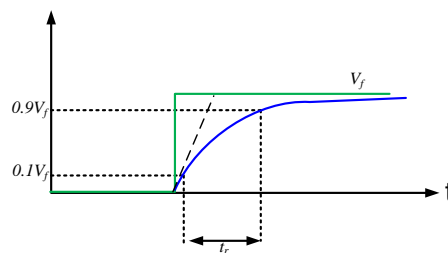
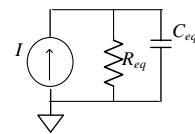
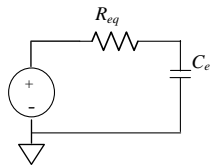
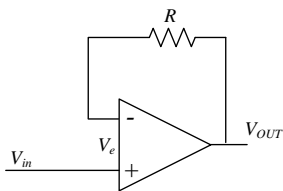
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Transient response Rise-time (ideal)





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